

## NOTE

## Partial Oxidation of Methane over Silica- and Alumina-Supported Vanadia Catalysts

A considerable effort has been made to study catalysts which are active and selective for the partial oxidation of methane to oxygenates primarily because of the need to convert surplus natural gas, mainly methane, to value added products (1, 2). Among the catalysts active and selective for partial oxidation, supported vanadia and molybdena catalysts have been shown to be the most promising (2–7). Although there have been a number of studies reporting on the influence of different vanadia species on the activity and selectivity for the partial oxidation of higher hydrocarbons (8–12), including ethane (13, 14), such investigations have not yet been made for the partial oxidation of methane. In a companion article we reported on the nature of the vanadium species and the dispersion of vanadia found on  $V_2O_5/SiO_2$  and  $V_2O_5/Al_2O_3$  catalysts as determined by TPR and solid-state  $^{51}V$  NMR (15). In this note, we report on the influence of the nature of these species and the effect of vanadia dispersion on the activity and selectivity for the partial oxidation of methane.

$V_2O_5/SiO_2$  and  $V_2O_5/Al_2O_3$  catalyst having a loading of 1.5–25 wt%  $V_2O_5$  were prepared by standard wet impregnation starting from ammonium metavanadate. A detailed description of this preparation can be found elsewhere (15). After impregnation, the catalysts were ground to <400 mesh, dried overnight at 100°C, and calcined at 550°C for 8 h. The pure supports,  $SiO_2$  (Cab-O-Sil, Cabot Corp.) and  $\gamma-Al_2O_3$  (Vista Chemicals), were subjected to a similar preparation treatment. Bulk  $V_2O_5$  was bought from Aldrich and used as received. Dispersions of vanadia on silica- and alumina-supported  $V_2O_5$  catalysts, as estimated by TRP and reported in a separate publication, are given in Tables 1 and 2 (15).

The partial oxidation of methane was carried out in a quartz microreactor system described elsewhere (16). The reaction conditions used were  $P = 1$  atmosphere,  $T = 500$ – $650^\circ C$ , catalyst weight = 100–200 mg, total flow rate = 150  $cm^3/min$ ,  $CH_4$  flow rate = 108  $cm^3/min$ ,  $CH_4/O_2 = 10$ , and balance He. The catalyst was pre-treated for 1 h in  $O_2$  at 550°C before starting the flow of methane in the system. All effluent lines were heat traced to 150°C in order to prevent the polymerization of formal-

dehyde. The products were analyzed by online gas chromatography.

Bulk  $SiO_2$  and  $V_2O_5$  exhibited negligible activities in the temperature range (500–650°C) studied.  $Al_2O_3$  exhibited measurable activity for methane oxidation to CO and  $CO_2$  only above 600°C with CO and  $CO_2$  being the only products detected (see Table 2).

Formaldehyde, CO, and  $CO_2$  were the main products observed over the  $V_2O_5/SiO_2$  catalysts with  $CH_3OH$  and  $C_2H_6$  detected only in trace amounts. The methane conversion, selectivities, and reaction rates of the  $V_2O_5/SiO_2$  catalysts at 580°C are listed in Table 1. In all cases the conversions were limited to less than 5% in order to maintain differential conditions. Reaction rates on a total catalyst weight basis increased initially with increasing vanadia loading and then decreased. The same behavior was observed at all temperatures studied.

Based on the  $V_2O_5$  dispersion estimated by TPR (see Table 1), turnover frequencies (TOFs) were calculated. These are given in the form of an Arrhenius plot, shown in Fig. 1. Although some variations exist in the TOFs with a change in the loading, these are within experimental error. An apparent activation energy of  $190 \pm 20$  kJ/mol was determined. Thus the total rate of methane conversion based on surface V can be considered to be similar for all the  $V_2O_5/SiO_2$  catalysts. Similar observations have been reported for the oxidation of ethane over  $V_2O_5/SiO_2$  (13).

Figure 2 shows the HCHO selectivities as a function of methane conversion for the  $V_2O_5/SiO_2$  catalysts. In all cases, HCHO selectivity decreased with an increase in methane conversion and only approached 100% at very low conversions. Such behavior is typical of partial oxidation reactions where the selective products are the primary reaction products and the nonselective products are the result of secondary reactions (4, 17). For a given conversion, HCHO selectivity also decreased with an increase in  $V_2O_5$  loading above 4% vanadia loading. The difference in selectivity with  $V_2O_5$  loading may be attributed to changes in the structure of vanadia. We have shown earlier that the dispersion of vanadia decreased

TABLE 1

Conversions and Selectivities for the Partial Oxidation of Methane over  $V_2O_5/SiO_2$  Catalysts at 580°C

Catalyst	Dispersion estimated by TPR <sup>a</sup>	CH <sub>4</sub> Conv. (%) <sup>b</sup>	Selectivity (%)		Rate ( $\mu\text{mol/g s}$ ) <sup>c</sup>
			HCHO	CO <sub>x</sub>	
1.6% $V_2O_5/SiO_2$	60	0.5	75	25	4.0
4.0% $V_2O_5/SiO_2$	38	2.6	45	55	20.0
8.2% $V_2O_5/SiO_2$	17	1.3	28	72	10.4
25.0% $V_2O_5/SiO_2$	6	0.7	21	79	5.8

<sup>a</sup> From Ref. (15).

<sup>b</sup> For 100 mg of catalyst.

<sup>c</sup> Based on per gram of catalyst.

with an increase in the vanadia loading (15). This was due to an increase in the amount of bulk-like vanadia, whereas the amount of surface vanadia remained essentially constant for all the  $V_2O_5/SiO_2$  catalysts, on a constant total catalyst weight basis (15). Thus the decrease in the HCHO selectivity with an increase in vanadia loading may be attributed to a secondary reaction of formaldehyde on bulk-like vanadia. Recently, Bars *et al.* (14) reported a similar trend for the oxidation of ethane over  $V_2O_5/SiO_2$  catalysts wherein the nonselective products were favored at higher vanadia loadings.

In contrast with the silica-supported catalysts, the oxidation of methane over  $V_2O_5/Al_2O_3$  catalysts produced only CO and CO<sub>2</sub>. No HCHO or CH<sub>3</sub>OH could be detected under any of the conditions used in these experiments. Table 2 shows the methane conversion, selectivities, and the reaction rates at 560°C for this series of catalysts. In this case, the total rate of methane oxidation on a total catalyst weight basis increased with an increase in vanadia loading. When the rates are expressed in terms of a TOF (see Fig. 3) the 2%  $V_2O_5/Al_2O_3$  catalyst is noted

TABLE 2

Conversions and Selectivities for the Partial Oxidation of Methane over  $V_2O_5/Al_2O_3$  Catalysts at 560°C

Catalyst	Dispersion estimated by TPR <sup>a</sup>	CH <sub>4</sub> Conv. (%) <sup>b</sup>	Selectivity (%)		Rate ( $\mu\text{mol/g s}$ ) <sup>c</sup>
			HCHO	CO <sub>x</sub>	
$Al_2O_3$ <sup>d</sup>	—	0.6	—	100	2.0
2.0% $V_2O_5/Al_2O_3$	100	1.0	—	100	7.2
4.8% $V_2O_5/Al_2O_3$	100	1.1	—	100	8.0
8.9% $V_2O_5/Al_2O_3$	85	2.0	—	100	15.2

<sup>a</sup> From Ref. (15).

<sup>b</sup> For 100 mg of catalyst weight.

<sup>c</sup> Based on per gram of catalyst.

<sup>d</sup> At  $T = 600^\circ\text{C}$  and wt of catalyst = 200 mg.

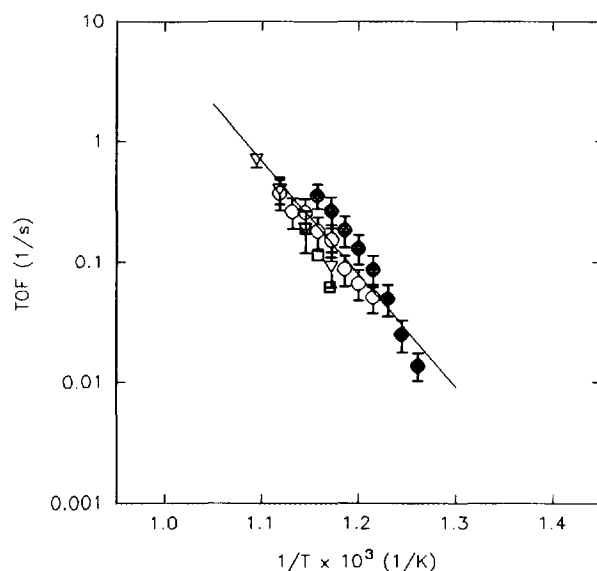


FIG. 1. Activity for the partial oxidation of methane over  $V_2O_5/SiO_2$  catalysts. ( $\nabla$ ) 1.6%, ( $\bullet$ ) 4.0%, ( $\circ$ ) 8.2%, and ( $\square$ ) 25%  $V_2O_5/SiO_2$ .

to be more active on a surface vanadia basis than either the 4.8 or the 8.9% loading catalysts. The activation energy for methane oxidation on the  $V_2O_5/Al_2O_3$  catalysts was calculated to be  $210 \pm 6$  kJ/mol.

The differences in the activities seen for these catalysts may be due to the differences in the types of V species present on the surface. Tetrahedral monomeric vanadia species tend to predominate at low vanadia loadings for the  $V_2O_5/Al_2O_3$  catalysts (18, 19). As the vanadia loading is increased, the vanadia species tends to polymerize, yielding dimeric, tetrameric, and finally polymeric surface species (15, 18, 19). Since the TOF for the 2%  $V_2O_5/Al_2O_3$  catalysts is higher than that for the higher loading catalysts, it is proposed that the monomeric vanadia present on the 2%  $V_2O_5/Al_2O_3$  catalyst is more active toward

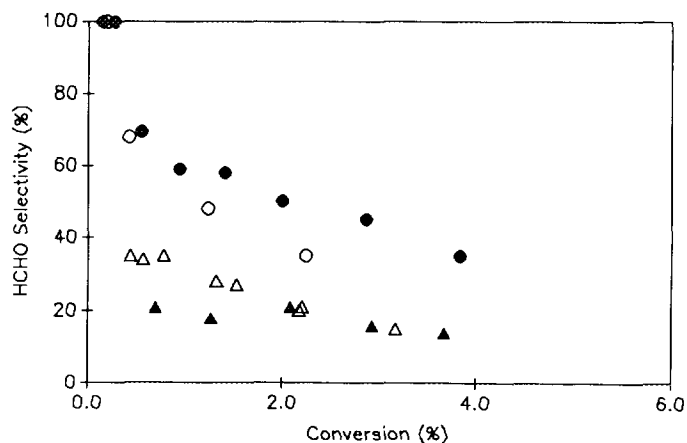


FIG. 2. CH<sub>4</sub> conversion vs HCHO selectivity for  $V_2O_5/SiO_2$  catalysts. ( $\circ$ ) 1.6%, ( $\bullet$ ) 4.0%, ( $\Delta$ ) 8.2%, and ( $\blacktriangle$ ) 25%  $V_2O_5/SiO_2$ .

methane oxidation than other surface forms of vanadia which can exist at higher loading. Indeed, Haber *et al.* (20) have reported that monomeric vanadia species are more easily reduced than dimeric forms which would suggest that the former is more active for methane oxidation.

The negligible activity exhibited by bulk  $V_2O_5$  cannot be simply attributed to its low surface area since the 25%  $V_2O_5/SiO_2$  catalyst, which has a similar  $V_2O_5$  surface area (15), was shown to be active for methane oxidation. This suggests that the active sites necessary for methane oxidation are somehow related to the structure of vanadia. Bulk  $V_2O_5$  is known to have an octahedral structure, whereas tetrahedral vanadia is present on silica- and alumina-supported vanadia (15, 18, 21). Thus it is proposed that a tetrahedral V species is an active site for methane oxidation on the supported catalysts. This is also confirmed by the fact that the TOF for  $V_2O_5/SiO_2$  was essentially invariant with  $V_2O_5$  loading. TOF was calculated based on a measurement of amount of surface vanadia estimated by TPR. That measurement correlated well with the amount of tetrahedral vanadia determined by NMR (15).

On the  $V_2O_5/Al_2O_3$  catalysts, no HCHO or  $CH_3OH$  was detected. This can be attributed either to differences in the nature of the  $V_2O_5$  sites or to active sites on the surface of the alumina. It was shown earlier that the nature of the surface vanadia is similar for silica- and alumina-supported vanadia as determined by NMR and TPR (15) and that on  $V_2O_5/Al_2O_3$  no bulk-like vanadia is present at low loadings. However, reduction during TPR of the surface vanadia on alumina appears to begin 20°C lower than that on  $SiO_2$ . This suggests that  $V_2O_5/Al_2O_3$  may be more prone to form the more oxidized products ( $CO_x$ ) than

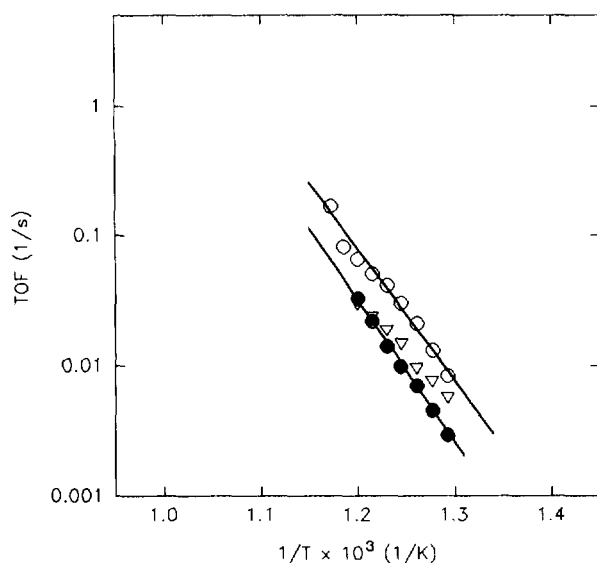


FIG. 3. Activity for the partial oxidation of methane over  $V_2O_5/Al_2O_3$  catalysts. (Error bars are proportional to the size of the symbols.) ( $\nabla$ ) 2.0%, ( $\bullet$ ) 4.8%, and ( $\circ$ ) 8.9%  $V_2O_5/Al_2O_3$ .

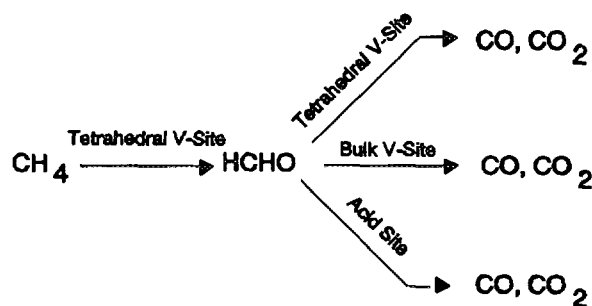


FIG. 4. Generalized reaction pathway for the partial oxidation of methane.

$V_2O_5/SiO_2$ . However, some formation of HCHO on the active vanadia sites cannot be completely ruled out. In order to test this hypothesis, dual bed experiments similar to those of Spencer and Pereira (4) were carried out in which the feed contacted first a bed of  $V_2O_5/SiO_2$  followed by a  $V_2O_5/Al_2O_3$  bed and vice versa. No HCHO was detected in the former case, whereas HCHO was readily detected in the latter. Similar observations were noted when plain  $Al_2O_3$  was used in place of the  $V_2O_5/Al_2O_3$ . Thus it is likely that, even if HCHO is initially formed on the tetrahedral vanadia sites on  $V_2O_5/Al_2O_3$ , it is further oxidized by acid sites on the alumina.

Based on these observations a generalized reaction pathway for  $V_2O_5/SiO_2$  and  $V_2O_5/Al_2O_3$  catalysts as shown in Fig. 4 can be written. H abstraction and oxygen insertion leading to the selective partial oxidation product, HCHO, appears to take place on a tetrahedral vanadia site. The HCHO so formed can then undergo secondary reaction on either bulk-like vanadia or on alumina acid sites resulting in the formation of the nonselective products, CO and  $CO_2$ . Thus proper control over readsorption sites is the key to controlling the selectivity in the partial oxidation of methane.

#### ACKNOWLEDGMENTS

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#### REFERENCES

1. Pitchai, R., and Klier, K., *Catal. Rev.-Sci. Eng.* **28**, 13 (1987).
2. Brown, M. J., and Parkyns, N. D., *Catal. Today* **8**, 305 (1991).
3. Spencer, N. D., *J. Catal.* **109**, 187 (1988).
4. Spencer, N. D., and Pereira, C. J., *J. Catal.* **116**, 399 (1989).
5. Liu, H. F., Liu, R. S., Liew, K. Y., Johnson, R. E., and Lunsford, J. H., *J. Am. Chem. Soc.* **106**, 4117 (1984).
6. Khan, M. M., and Somorjai, G. A., *J. Catal.* **91**, 263 (1985).
7. Otsuka, K., and Hanato, M., *J. Catal.* **108**, 252 (1987).
8. Fierro, J. L. G., Gambaro, L. A., Cooper, T. A., and Kremenec, G., *Appl. Catal.* **6**, 363 (1983).
9. Bond, G., Zurita, J. P., Flamerz, S., Gellings, P. J., Bosch, H., Ommen, J. G. V., and Kip, B. J., *Appl. Catal.* **22**, 361 (1986).

10. Wachs, I. E., Saleh, R. Y., Chan, S. S., and Cherisch, C. C., *Appl. Catal.* **15**, 339 (1985).
11. Lopez Nieto, J. M., Kremenec, G., and Fierro, J. L. G., *Appl. Catal.* **61**, 235 (1990).
12. Bond, G., and Tahir, S. F., *Appl. Catal.* **71**, 1 (1991) and references therein.
13. Oyama, S. T., and Somarjai, G. A., *J. Phys. Chem.* **94**, 5022 (1990).
14. Bars, J. L., Vedrine, J. C., Auroux, A., Trautmann, S., and Baerns, M., *Appl. Catal. A: General* **88**, 179 (1992).
15. Koranne, M. M., Goodwin, J. G., Jr., and Marcelin, G., *J. Catal.* **148**, 369 (1994).
16. Lo, M. Y., Agarwal, S. K., and Marcelin, G., *J. Catal.* **111**, 168 (1988).
17. Koranne, M. M., Goodwin, J. G., Jr., and Marcelin, G., *J. Phys. Chem.*, **97**, 673 (1993).
18. Vuurman, M. A., and Wachs, I. E., *J. Phys. Chem.* **96**, 5008 (1992) and references therein.
19. Went, G. T., Oyama, S. T., and Bell, A. T., *J. Phys. Chem.* **94**, 4240 (1990).
20. Haber, J., Kozolowski, A., and Kozolowski, R., *J. Catal.* **102**, 52 (1986).
21. Deo, G., Hardcastle, F. D., Richards, M., Hirt, A. M., Wachs, I. E., in "Novel Materials in Heterogeneous Catalysis" (R. T. Baker and L. L. Murrell, Eds.), ACS Symposium Series" Vol. 437, p. 317. Amer. Chem. Soc., Washington, DC, 1990.

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